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An uncertainty-based approach**

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Optimizing mining complexes with multiple processing and transportation alternatives: An uncertainty-based approach

Luis Montiel
Roussos Dimitrakopoulos

GERAD & COSMO – Stochastic Mine Planning Laboratory, Department of Mining and Materials Engineering, McGill University, Montréal (Québec) Canada H3A 0E8

luis.montiel@mail.mcgill.ca
roussos.dimitrakopoulos@mcgill.ca

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Abstract: Mining complexes contain multiple sequential activities that are strongly interrelated. Extracting the material from different sources may be seen as the first main activity, and any change in the sequence of extraction of the mining blocks modify the activities downstream, including blending, processing and transporting the processed material to final stocks or ports. Similarly, modifying the conditions of operation at a given processing path or the transportation systems implemented may affect the suitability of using a mining sequence previously optimized. This paper presents a method to generate mining, processing and transportation schedules that account for the previously mentioned activities (or stages) associated with the mining complex simultaneously. The method uses an initial solution generated using conventional optimizers and improves it by mean of perturbations associated to three different levels of decision: block based perturbations, operating alternative based perturbations and transportation system based perturbation. The method accounts for geological uncertainty of several deposits by considering scenarios originated from combinations of their respective geostatistical orebody simulations.

The implementation of the method in a multipit copper operation shows its ability to reduce deviations from capacity and blending targets while improving the expected NPV, which highlight the importance of stochastic optimizers given their ability to generate more value with less risk.

Key Words: Mining complex, geostatistical orebody simulations, operating alternatives.

1 Introduction

A mining complex can be interpreted as a supply chain system where material is transformed from one activity to another (Goodfellow and Dimitrakopoulos, 2012). The primary activities (or stages) consist of: (i) mining the materials from one or multiple sources (deposits); (ii) blending the material considering stockpiling, (iii) processing the material in different processing paths, and, at each path, account for multiple operating alternatives; and (iv) transporting the products to port of final stocks using one or multiple transportation systems.

For a given processing path (e.g. mill-roaster in a refractory ore operation), it is possible to have multiple operating alternatives; for example, a mill may be operated using two different options: fine or coarse grinding (Fig. 1). If the mill is operated using fine grinding, there is often a very high energy consumption, which is associated with a higher processing cost and also requires larger residence times for the material processed, thus limiting the mill throughput. A coarse grinding option requires less energy and residence time in the mill, which decreases the operating cost and increases the mill throughput, however, it results in a lower recovery in the roaster downstream. Furthermore, different processing alternatives often impose different blending requirements. For example, the tolerable amount of free silica of the input material may be lower when operating the mill at fine grinding given that the presence of this element increases the hardness of the material. Case studies have demonstrated (Whittle, 2011) that for maximizing the net present value (NPV) when a mill is bottlenecking the system, it is better to use a coarse grind with higher throughput in the early periods of the life-of-mine (LOM), and, to use a finer grind to maximize recovery towards the end of the LOM. During the early periods, a mining complex incurs an opportunity cost for having material with large residence times in the mill, however, as the quantity of ore remaining in the mining complex diminishes, there is no opportunity cost.

Once the material is processed through the different processing paths and using some available operating alternatives, existing transportation systems, either continuous (belt conveyors, pipe transport) or batch (trucks, rail transportation), are used to transport the processed material to one or several ports or final stocks. Accounting for transportation systems in the optimization of mining complexes is important, given that they may limit the overall system output. In a mining complex, it is common to have multimodal transportation that involves the use of separate contractors or operators for each type of transport (Zamorano, 2011). To account for the demand of transportation of material processed, it is necessary to establish the feasible relations between processing paths and transportation systems; specifically, a particular transportation system may be able to handle output material from some of the available processing paths: For example, in a pyro/hydrometallurgical complex, a hydraulic pipe may be able to transport the material output from the leaching plant whereas the material output from the pyrometallurgical plant is transported to the final stocks via trucks. Once the feasible transport relations are established, the demand for transportation is evaluated by considering the throughput relationships (output/input tonnages) for each processing path given the operating alternative implemented. For example, the output/input tonnage relation and the metallurgical recovery in a gold flotation plant change if the mass pull is 4 or 7% (Hadler et al., 2010). When the transportation of processed material is the bottleneck in the overall system, the operating conditions at the different processing paths must be evaluated. To overcome this limitation, it may be useful to re-evaluate throughput specifications of the processed material. Whittle (2011) shows that by increasing the copper concentrate from 28 to 32% in some periods on a sulphide deposit, the metallurgical recovery decreases by 7%, but the NPV increases by 6% given the possibility of transporting more concentrated ore on the pipe, which is the bottleneck of the system.

Optimizing mining complexes by considering geological uncertainty and the different stages simultaneously is a large combinatorial optimization problem. Several efficient methodologies have been developed in stochastic environments for the mine production scheduling problem (Godoy, 2003; Godoy and Dimitrakopoulos, 2004; Lamghari and Dimitrakopoulos, 2012; Lamghari et al. 2012) and blending optimization (Asad and Dimitrakopoulos, 2012; Goodfellow and Dimitrakopoulos, 2012). This paper presents a methodology for optimizing the mine plan and destination and transportation policies by considering all the stages of the mining complex simultaneously, and accounting for geological uncertainty by means of geostatistical orebody simulations of the deposit(s). The next section presents the formulation of the problem and the

heuristic methodology proposed to solve it. Then, its implementation at a multi-pit operation is described; and, finally, some conclusions and future research avenues are addressed.

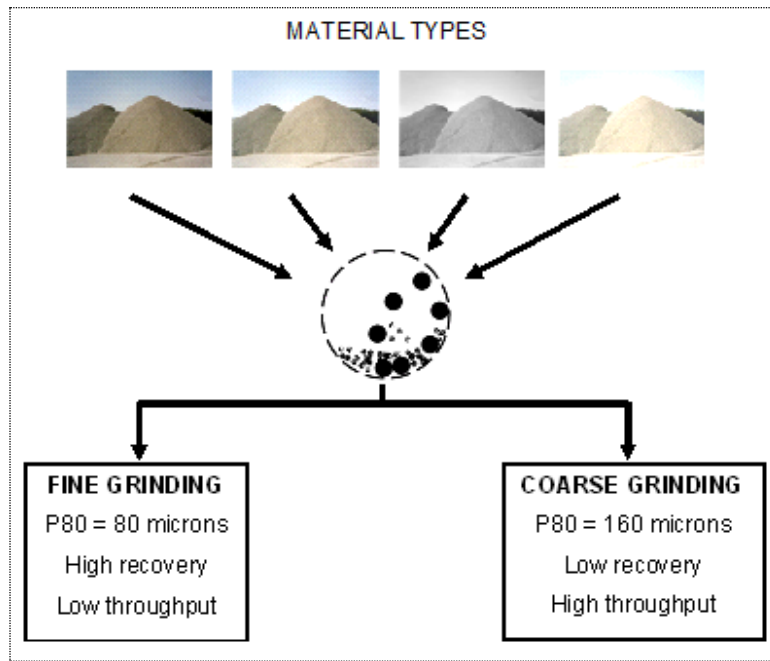


Figure 1: Operating alternatives for a mill

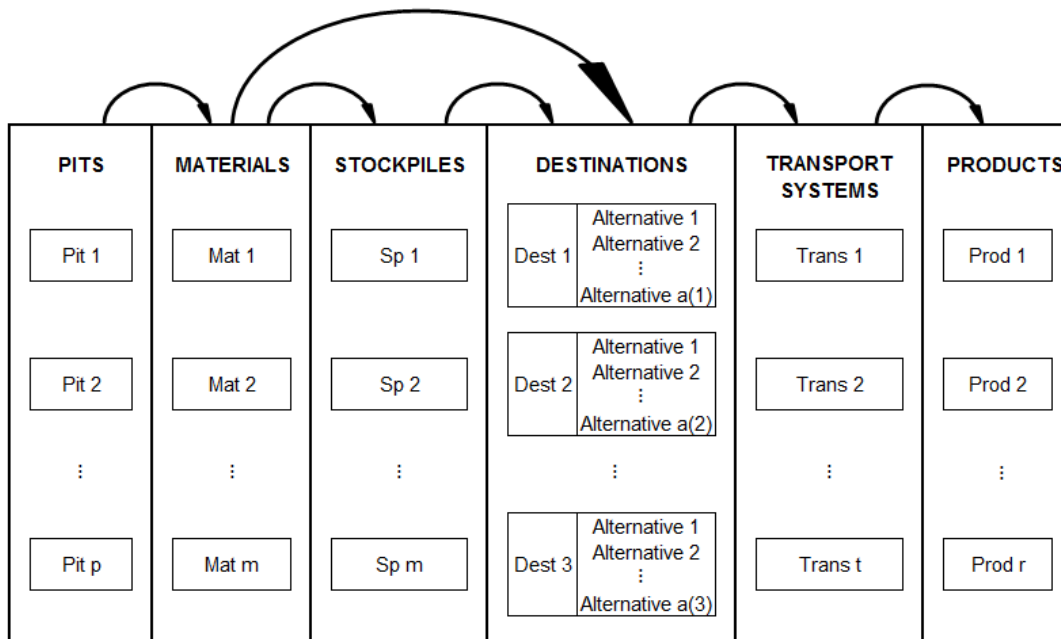


Figure 2: Flexibility of the mining complex

2 Method

2.1 Overview

In a mining complex, the material flows from the deposits as raw material to ports or final stocks as saleable products. To optimize the mining complex, the different stages that are involved must be considered simultaneously (Fig. 3).

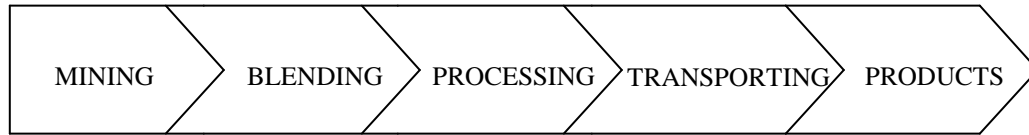


Figure 3: Stages of the mining complex

First, the multiple material types coming from the mine(s) are sent to the available processes or to stockpiles where they are blended to meet the quality requirements. At each process the material is transformed into intermediate or final products, which are then transported to port(s) or final stocks. The goal when optimizing a mining complex is to maximize discounted cash flows while minimizing deviation from mining and metallurgical processing targets, such as capacities associated to the different processing and transportation options and blending requirements regarding the different metallurgical properties. These metallurgical properties control the operation of the different processes and are calculated as mathematical expressions of the different grade elements, e.g., fuel value is a metallurgical property that controls the operation on a roaster. The formulation of the problem is given in the next section, and the approach proposed in Section 2.3.

2.2 Optimization model

2.2.1 Sets, variables and parameters

Sets

- S: set of scenarios obtained from geological orebody simulations of the deposit(s)
- T: set of periods considered in the LOM
- P: set of mining pits
- I: set of mining blocks considering all available pits
- D: set of destinations (processing paths) available
- O(d): set of operating alternatives at destination d
- M: set of grade elements (including recoverable metals)
- K: set of metallurgical properties
- R: set of transportation systems

Variables

- X_{itd} : binary variable denoting whether or not a block i is mined in period t and sent to destination d
- Y_{tdo} : binary variable denoting whether or not a processing alternative o is implemented in destination d in period t
- Z_{tdr} : linear variable $\in [0, 1]$ that represents the proportion of output tonnage from destination d to be transported by transportation system r in period t
- $D(s, t, p)_U$: tonnage exceeding the capacity associated with pit p in period t under scenario s
- $D(s, t, p)_L$: deficient amount of tonnage mined in pit p during period t under scenario s regarding its associated capacity

- $D(s, t, d, o)_U$: tonnage exceeding the capacity associated with the operation alternative o of destination d in period t considering the scenario s
- $D(s, t, d, o)_L$: deficient amount of tonnage input to destination d in period t under scenario s considering operating alternative o and its associated capacity
- $D(s, t, d, o, k)_U$: over-deviation from the upper target regarding the metallurgical property k in processing option o of destination d in period t under scenario s
- $D(s, t, d, o, k)_L$: under-deviation from the lower target regarding the metallurgical property k in processing option o of destination d in period t under scenario s
- $D(s, t, r)_U$: tonnage exceeding the capacity associated with the transportation system r in period t considering the scenario s
- $D(s, t, r)_L$: deficient amount of tonnage regarding the capacity associated with transportation system r in period t under scenario s
- $discprofit(s, t)$: discounted profit obtained in period t under scenario s
- $revenue(s, t)$: revenue in period t under scenario s
- $mncst(s, t)$: cost of mining the materials in period t under scenario s
- $procst(s, t)$: cost of processing the materials in period t under scenario s
- $stkst(s, t)$: cost of stockpiling the materials in period t under scenario s
- $rhandlecst(s, t)$: cost of sending material from the stockpiles to the available destinations in period t under scenario s
- $transcst(s, t)$: cost of transporting the products to the ports or final stocks in period t under scenario s
- $penalty(s, t)$: penalty term of objective function in period t under scenario s
- $penalpitcap(s, t)$: penalized deviations from pits capacities in period t under scenario s
- $penalprocap(s, t)$: penalized deviations from operation alternatives capacities in period t under scenario s
- $penalprometal(s, t)$: penalized deviations from metallurgical operational ranges in period t under scenario s
- $penaltranscap(s, t)$: penalized deviations from transportation systems capacities in period t under scenario s
- $mnproduction(s, t)$: tonnage mined in period t under scenario s
- $tonnesentmn(s, t, d)$: tonnage sent from the pits to destination d in period t under scenario s
- $tonnestockpiles(s, t)$: tonnage presented in the stockpiles in period t under scenario s
- $tonnerehandle(s, t, d)$: tonnage sent from the stockpiles to destination d in period t under scenario s
- $tonneprocess(s, t, d)$: tonnage of material processed in destination d in period t under scenario s
- $metalsentmn(s, t, d, m)$: amount of metal m sent from the pits to destination d in period t under scenario s
- $metalorehandle(s, t, d, m)$: amount of metal m sent from the stockpiles to destination d in period t under scenario s
- $metalsemtmn(s, t, d, m)$: amount of metal m input to destination d in period t under scenario s
- $tonneoutprocess(s, t, d)$: tonnage of material output from destination d in period t under scenario s
- $tonnetransport(s, t, r)$: tonnage of material transported using transportation system r in period t under scenario s
- $metalrec(s, t, m)$: amount of metal m recovered in period t under scenario s

Parameters

- m_{is} : mass of block i under scenario s
- P_{do} : proportion output/input tonnage in operation alternative o of destination d
- A_{dr} : 0-1 parameter indicating whether or not the output material from destination d can be transported using transportation system r (feasible relationships)

- $rec(d, o, m)$: metallurgical recovery of metal m in destination d using the operation alternative o
- $price(m)$: price of metal m
- m_c : per-unit mining cost
- $p_c(d, o)$: per-unit processing cost in destination d using operation alternative o
- k_c : per-unit stockpiling cost
- h_c : per-unit rehandle cost
- $\tau_c(r)$: per-unit transportation cost using transportation system r
- $drate$: discount rate
- $C(t, p)_U$: per-unit penalty cost associated with over-deviation of production in pit p during period t
- $C(t, p)_L$: per-unit penalty cost associated with under-deviation of production in pit p during period t
- $C(t, d, o)_U$: per-unit penalty cost associated with over-deviation of production in operation alternative o of destination d during period t
- $C(t, d, o)_L$: per-unit penalty cost associated with under-deviation of production in operation alternative o of destination d during period t
- $C(t, d, o, k)_U$: per-unit penalty cost associated with over-deviation from upper target of metallurgical property k in period t considering operation alternative o of destination d
- $C(t, d, o, k)_L$: per-unit penalty cost associated with under-deviation from lower target of metallurgical property k in period t considering operation alternative o of destination d
- $C(t, r)_U$: per-unit penalty cost associated with exceeding the capacity of transportation system r during period t
- $C(t, r)_L$: per-unit penalty cost associated with failing to meet the tonnage capacity of the transportation system r during period t

2.2.2 Objective function

The objective function is given by Eq. (1) and seeks for maximizing discounted profits and minimizing deviations from targets along all periods and scenarios (derived from orebody simulations). The first term of the objective function accounts for discounted profits by evaluating the revenues obtained by selling the different products and the costs associated to the different stages of the mining complex. The second term accounts for penalized deviations regarding mining, processing, transporting and blending targets and may be seen as a penalty cost it is incurred by not meeting the different targets. The value of $penalty(s, t)$ depends on the deviations from the targets itself and the magnitude of the per-unit penalty costs associated. If the per-unit penalty costs are too high, the method will improve the reproduction of the targets ignoring the first term of the objective function generating poor improvement of expected NPV. Conversely, too small per-unit penalty costs will generate impractical solutions with large and non-realistic NPV forecasts given the high violations of the targets.

$$MaxO = \sum_{t=1}^T \left[\frac{1}{S} \left(\sum_{s=1}^S discprofit(s, t) - penalty(s, t) \right) \right] \quad (1)$$

To manage the risk along the different periods, the per-unit penalty costs can be discounted using the geological risk discounting rate (GRD) introduced by Dimitrakopoulos and Ramazan (2004). This allows deferring risks of not meeting targets for later periods when more information will be available. GRD can be applied to processing, blending and transporting targets.

2.2.3 Model constraints

When generating a strategic plan for a mining complex there are important questions that need to be answered: (i) at each mining block, when to mine it and where to send it; (ii) at each destination (processing path), which processing alternative to implement every period; (iii) which transportation systems should

be used to transport the products. Any particular solution, independent of its quality, must answer these questions.

The tonnage mined in a given period t under a scenario s can be evaluated as:

$$mnproduction(s, t) = \sum_{i=1}^I \sum_{d=0}^D X_{itd} \cdot m_{is} \quad (2)$$

Scenarios are obtained from orebody simulations and, due to grade and material type uncertainties, the tonnage of a block may differ from one scenario to another. Similarly, the tonnage sent from the pits to any particular destination d can be evaluated as:

$$tonnesentmn(s, t, d) = \sum_{i=1}^I X_{itd} \cdot m_{is}, \quad (3)$$

In a mining complex, different material types are storage in different stockpiles given that they may have different metallurgical properties. The model considers one stockpile for each material type that contributes to the blending operation. When a particular block is sent to the stockpiles, the assignment of any particular stockpile is a scenario-dependent decision derived from the material type uncertainty. In other words, for each scenario, a stockpiled block will be assigned to the corresponding pile related to its material type. For modeling purposes, stockpiling a block is represented as having destination $d = 0$. Therefore, in a period t , the total tonnage presented in the stockpiles under a scenario s is:

$$tonnestockpiles(s, t) = tonnestockpiles(s, t - 1) + tonnesentmn(s, t, 0) - \sum_{d=1}^D tonnerhandle(s, t, d) \quad (4)$$

The amount of material processed in a given destination d during period t under scenario s is given by:

$$tonneprocess(s, t, d) = tonnesentmn(s, t, d) + tonnerhandle(s, t, d) \quad (5)$$

Similarly, the amount of metal m input to a particular destination d during period t under scenario s can be evaluated as:

$$metalprocess(s, t, d, m) = metalsentmn(s, t, d, m) + metalrehandle(s, t, d, m) \quad (6)$$

At any given period t , only one of the possible available operating alternatives $o(d)$ can be implemented in a particular destination d , which implies that:

$$\sum_{o=1}^{O(d)} Y_{tdo} = 1 \quad (7)$$

At each destination, every available operating alternative may have its corresponding associated capacity, operating cost, recoveries, operational ranges for metallurgical properties, and throughput specification (relation between output/input tonnages). The amount of material output from a given destination d in period t under scenario s is given by:

$$tonneoutprocess(s, t, d) = \sum_{o=1}^{O(d)} (tonneprocess(s, t, d) \cdot Y_{tdo} \cdot P_{do}) \quad (8)$$

After evaluating the output material from the different destinations in a period t under scenario s , the tonnage transported by a given transportation system r can be calculated as:

$$tonnetransport(s, t, r) = \sum_{d=1}^D (tonneoutprocess(s, t, d) \cdot Z_{tdr}) \quad (9)$$

Eq. (10) and (11) are used to respect feasible process-transport configurations and transport all output material obtained from a given destination.

$$Z_{tdr} \leq A_{dr}, \quad \forall t, d, r \quad (10)$$

$$\sum_{r=1}^R Z_{tdr} = 1, \quad \forall t, d \quad (11)$$

The amount of metal m recovered in period t under scenario s can be calculated as:

$$metalrec(s, t, m) = \sum_{d=1}^D \sum_{o=1}^{O_d} (metalprocess(s, t, d, m) \cdot rec(d, o, m)) \quad (12)$$

Using the amount of metals recovered, it is possible to calculate the revenue obtained in period t under scenarios s as:

$$revenue(s, t) = \sum_{m=1}^M metalrec(s, t, m) \cdot price(m), \quad (13)$$

The costs associated with the different stages of the mining complex are given by Eq. (14)–(18):

$$mncst(s, t) = mnproduction(s, t) \cdot m_c, \quad \forall s, t \quad (14)$$

$$procst(s, t) = \sum_{d=1}^D \sum_{o=1}^{O_d} (tonneprocess(s, t, d) \cdot p_c(d, o) \cdot Y_{tdo}), \quad \forall s, t \quad (15)$$

$$stkst(s, t) = tonnesentmn(s, t, 0) \cdot k_c, \quad \forall s, t \quad (16)$$

$$rhandlscst(s, t) = \left(\sum_{d=1}^D tonnerhandle(s, t, d) \right) \cdot h_c, \quad \forall s, t \quad (17)$$

$$transcst(s, t) = \sum_{r=1}^R (tonnetransport(s, t, r) \cdot \tau_c(r)), \quad \forall s, t \quad (18)$$

The discounted profit, which is the term that appears in the objective function, can be calculated by discounting the difference between the revenue and the costs associated with the different stages (Eq. (19)).

$$discprofit(s, t) = \frac{\left(\begin{array}{l} revenue(s, t) - mncst(s, t) - procst(s, t) - stkst(s, t) - \\ rhandlscst(s, t) - transcst(s, t) \end{array} \right)}{(1 + drate)^t} \quad (19)$$

To control the operations at the different destinations (processing paths), various metallurgical properties must be considered. At any given operation alternative of a particular destination, these metallurgical properties must fall in between some operational ranges. The deviations from these operational ranges must be also minimized by means of penalty costs.

$penalty(s, t)$ is the second term of the objective function and can be evaluated in each period and scenario using Eq. (20).

$$penalty(s, t) = penalpitcap(s, t) + penalprocap(s, t) + penalprometal(s, t) + penaltranscap(s, t) \quad (20)$$

The evaluation of the different penalized deviations that affect the penalty term of the objective function is displayed in Eq. (21)–(24).

$$penalpitcap(s, p) = \sum_{p=1}^P (C(t, p)_U \cdot D(s, t, p)_U + C(t, p)_L \cdot D(s, t, p)_L) \quad (21)$$

$$penalprocap(s, t) = \sum_{d=1}^D \sum_{o=1}^{O(d)} (C(t, d, o)_U \cdot D(s, t, d, o)_U + C(t, d, o)_L \cdot D(s, t, d, o)_L) \quad (22)$$

$$penalprometal(s, t) = \sum_{d=1}^D \sum_{o=1}^{O_d} \sum_{k=1}^K (C(t, d, o, k)_u \cdot D(s, t, d, o, k)_u + C(t, d, o, k)_l \cdot D(s, t, d, o, k)_l) \quad (23)$$

$$penaltranscap(s, t) = \sum_{r=1}^R (C(t, r)_u \cdot D(s, t, r)_u + C(t, r)_l \cdot D(s, t, r)_l) \quad (24)$$

The production and transportation capacities and the blending targets are controlled via penalties in the objective function. Other operational constraints, although not displayed in this paper, are considered in the formulation, such as precedence constraints, reserve constraints, etc. (Dimitrakopoulos and Ramazan, 2004).

2.3 Solution approach – simulated annealing

Given the complexity of the problem derived from the flexibility considered at the different stages of the mining complex, the use of an exact method incorporated in any conventional optimization software, such as CPLEX, will not be suitable as solution times will be impractical even for small instance problems (few thousands of blocks). To overcome this situation, a heuristic methodology is proposed to generate good-quality solutions. The proposed algorithm perturbs an initial solution iteratively to improve the objective function. In order to avoid local optimal solutions and to explore the solution domain (the set of all possible mine production schedules with operating policies for processing paths and transportation systems), the method allows deterioration based on a decision rule and uses diversification. The decision rule is the same implemented by the Metropolis algorithm (Metropolis et al., 1953) and allows the exploration of the solution domain while converging to a final good-quality solution. A diversification strategy over the solution domain is performed by means of perturbation at different stages of the mining complex (blocks, operating alternatives, transportation systems). The proposed algorithm can be implemented multiple times to improve the final solution by controlling the number of cycles.

2.3.1 Decision rule

Metropolis et al. (1953) introduce an algorithm to provide a simulation of a collection of atoms in equilibrium at a given temperature. The Metropolis algorithm perturbs the initial state and, at each iteration, an atom is displaced and the resulting change in energy ΔE is computed. If $\Delta E \leq 0$, the displacement is accepted. The case $\Delta E > 0$ is accepted or rejected based on random sampling of a probability distribution $P(\Delta E) = \exp(-\Delta E/k_B T)$ where k_B is a constant and T the temperature of the state. Kirkpatrick et al. (1983) use a cost function in place of the energy and define configurations by a set of variables to generate a population of configurations of a given optimization problem at some temperature. This temperature acts as a control parameter of the same units as the cost function. Previous implementation of annealing schedule have demonstrated its ability to improve mine production scheduling and pit designs in terms of expected NPV and meeting production targets (Godoy, 2003; Leite and Dimitrakopoulos, 2007; Albor and Dimitrakopoulos, 2009; Montiel and Dimitrakopoulos, 2011; Goodfellow and Dimitrakopoulos, 2013).

Given the nature of the optimization problem considered in this paper, which is a maximization problem and not a cost or deviation minimization one, a perturbation that deteriorates the current solution is the one that decreases its objective value. Accounting for this, the probability distribution is given by Eq. (25) with T being the annealing temperature.

$$P(\Delta O) = P(O_{new} - O_{current}) = \begin{cases} 1 & \text{if } (\Delta O \geq 0) \\ e^{-\frac{(\Delta O)}{T}} & \text{if } (\Delta O < 0) \end{cases} \quad (25)$$

The probability of accepting an unfavourable perturbation is greater at higher temperatures. As the optimization proceeds, the temperature is gradually lowered by a reduction factor. When the temperature approaches 0, the probability of accepting an unfavourable swap tends to zero. This allows the algorithm to converge to a final solution.

The total number of swaps and the number of swaps at a given temperature control the end of the algorithm and the changes of temperature throughout the iteration process.

2.3.2 Perturbation mechanism

The proposed algorithm requires an initial mining sequence to assign periods and destinations to mining blocks and a set of orebody simulations for each deposit to evaluate profits, costs, productions and deviations at the different stages of the mining complex. While reading the orebody simulations, the algorithm evaluates the overall profitability of a block at a given destination by accumulating the economic value of the block in that destination through all scenarios. For simplicity, the overall profitability of a block at a given destination will be referred to as OPBD. Based on the OPBD, it is possible to determine the optimal destination of a given block. One or several waste dumps may be considered and they are treated as processing destinations with null recoveries.

The solution is improved by means of the perturbation mechanism. The algorithm performs perturbation at three different level or stages: blocks, operating alternatives and transportation systems. At any level of perturbation, a new solution will be accepted based on the decision rule explained in the previous section.

2.3.3 Block based perturbation (BBP)

The algorithm selects a block randomly and checks its OPBD in the different destinations. It perturbs the solution by modifying periods and destinations of mining blocks. Moving the extraction period of a mining block to a previous period will be referred to as pulling up the block, whereas moving the block to a following period is referred to as pushing down the block. If the block has a positive OPBD in the optimal destination, the algorithm iterates the candidate period from a previous to a following period, favouring first the chance of pulling up the block given the time value of money. In the case where a block has negative OPBD in all destinations, the algorithm iterates from the following period without to the previous period, favouring first pushing down the block (Fig. 4). Before accepting any candidate period, the algorithm checks that slope constraints are respected.

For a block with positive OPBD in its optimal destination, the set of candidate destinations are those with positive OPBD. The algorithm sorts candidate destinations based on the OPBD and iterates from the most profitable destination to the less profitable one (but still with positive OPBD). If the block has negative OPBD in all destinations, the only candidate destination is its optimal destination (the one with higher OPBD). This ensures that waste blocks are always sent to the waste dump(s) as they are treated as destinations with null recoveries. There may be cases where blocks have negative OPBD in all destinations but the optimal destination is not a waste dump; that is, although processing that block in a particular processing path generates a negative profit, the profit losses are less by processing the block than by sending it to a waste dump. In these cases, optimal destinations are also respected.

Although, pulling up a positive block and pushing down a negative one improve NPV expectations because of the time value of money, the objective value of the new solution generated does not necessarily increase as there is a penalty term also affecting the objective function. There may be cases where the NPV increases, but the new solution deteriorates the objective value due to the penalized deviations. A similar analysis can be made for the opposite case; a perturbation that decreases NPV expectations does not necessarily deteriorate the current solution. The objective value can be seen then as a trade-off between improving the NPV and decreasing deviation from operational targets.

2.3.4 Operating alternative based perturbation (OBP)

In the previous section, block based perturbations were described; however, the operating alternatives implemented at each destination are not simultaneously modified. The set of perturbations at the OBP level

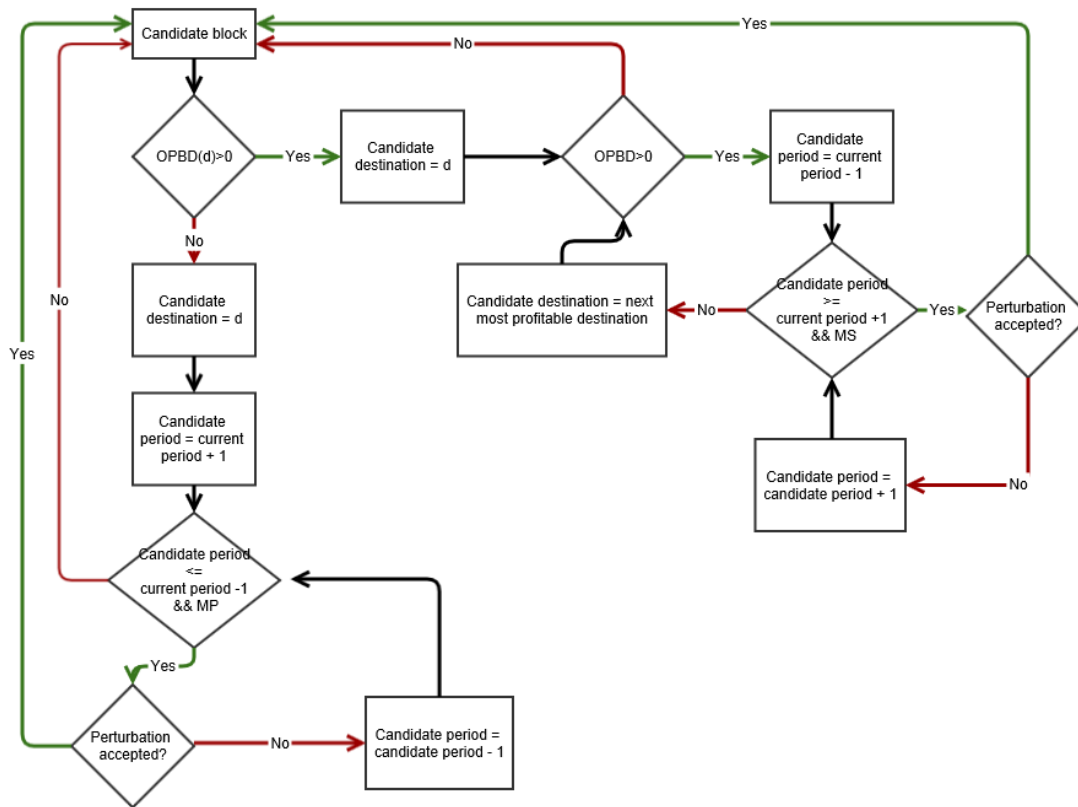


Figure 4: Block based perturbation

refer to swapping operating alternatives at the different destinations (processing paths); e.g., swapping from fine to coarse grinding in the mill in some periods of the LOM. Modifying the operating alternative at a particular destination in a given period may vary the objective value as:

- Processing cost and recovery may change, which may affect the expected NPV
- Capacity and operational metallurgical ranges may change, which affect the penalty term in the objective function

Given a particular period and destination, the algorithm selects randomly an available operating alternative as the candidate alternative, and evaluates the objective value when swapping the operating alternative to the candidate one (Fig. 5). The new solution is accepted or rejected based on the decision rule explained previously.

2.3.5 Transportation system based perturbation (TBP)

As previously explained, the first level of perturbations modify period and destinations of mining blocks, whereas the second level of perturbations modify operating alternatives at the different periods and destinations. The third level of perturbations is referred to as the transportation system based perturbations. For a given destination and period, the algorithm attempts to perturb the proportion of output material transported using the available transportation systems; e.g., the mill-roaster processing path (destination) change its transportation arrangement for the output material from [70% trucks / 30% pipe] to [50% trucks / 50% pipe]. This set of perturbations seeks to minimize the transportation costs and penalized deviations in the objective function. The variations of the proportions of transportation systems utilized are generated using random numbers but ensuring that 100% of the output material from a given destination is transported using the feasible transportation systems (mass conservation). Perturbations are accepted or rejected based on the decision rule previously explained.

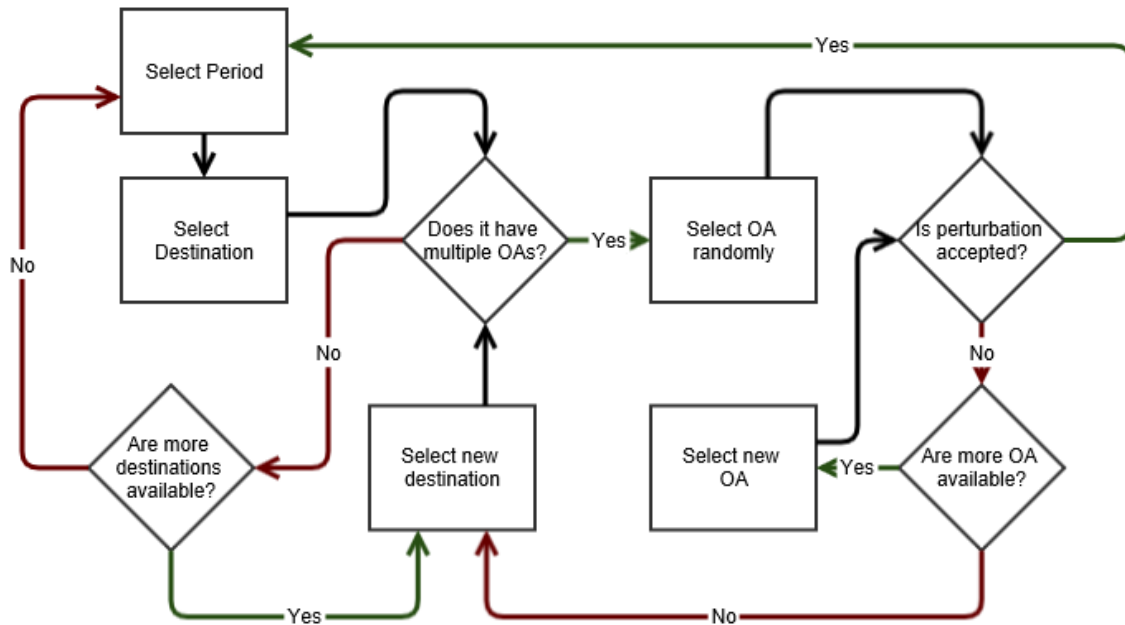


Figure 5: Operating alternative based perturbation

2.3.6 Integrating perturbations: The heuristic approach

The different stages of a mining complex are strongly interrelated. Any modification in a particular stage modifies the optimal operation at the other stages of the mining complex; e.g., modifying the mining sequence affects the optimal operating parameters at a given destination and the transportation system implemented. The same occurs when modifying operating parameters or transportation arrangements. Given the interrelation between the different stages, the algorithm integrates the multilevel perturbations in an iterative way (Fig. 6).

At any given temperature, a user-defined number of BBP is performed, when it reaches this predefined number, the temperature in this level of perturbation is lowered and the OBP starts. Similarly, when it reaches a user-defined number of OBP, the temperature in this level of perturbation is lowered and the TBP starts. When the three levels of perturbations are performed, the algorithm returns to the first level (BBP). It continues until the total number of BBP is reached.

The heuristic approach can be implemented iteratively by controlling the number of cycles. However, it must be important to establish a trade-off between the quality of the solution and computational time, given that it increases linearly with the number of cycles. Furthermore, there may be a number of cycles from where no significant improvement in the objective value of the solution is obtained.

3 Implementation of the method: A multi-pit operation

3.1 Overview of operation

The method is implemented in a mining complex that produces copper and contains two different pits: Pit A and Pit B. The material extracted from both pits has been classified in 5 different types that originate different metal recoveries at the different destinations. 5 destinations are available (Fig. 7), including a waste dump.

Twenty orebody simulations of each deposit are used, which consider both uncertainty in grades and material types. Three variables of interest are considered in the orebody simulations: copper, which is the

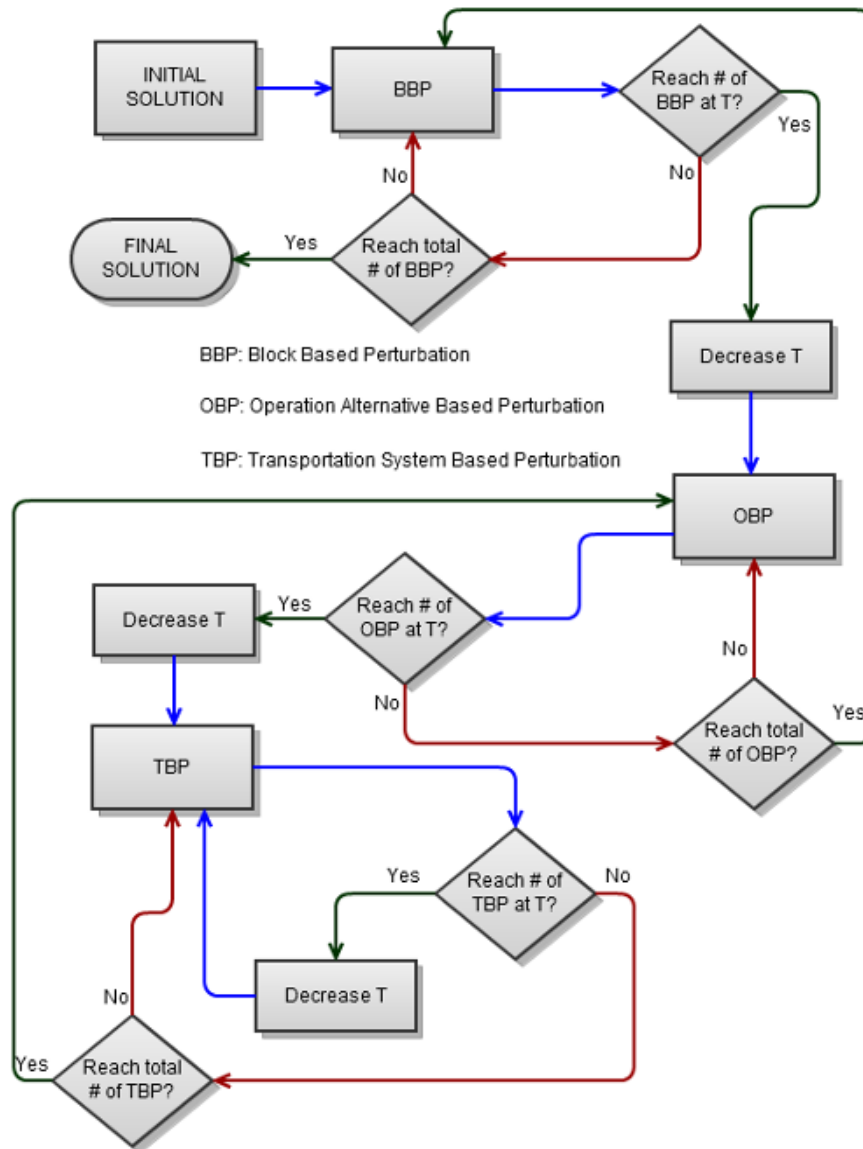


Figure 6: The heuristic approach

selling product of the mining complex; and two metallurgical properties that control the operation in the small and the big mill.

3.2 Base case

An initial solution for the multipit – multiprocess problem is generated using Whittle software. This initial solution contains the periods and destinations of mining blocks for both pits, and is generated considering the estimated geological models (E-types) of the two deposits; that is, the average grade of each block from the available simulations. This solution will be referred to as base case schedule and it is generated using a conventional optimizer widely used in the mining industry.

The results obtained by implementing the base case schedule are depicted in Fig. 8. Large and impractical deviations in terms of capacities and blending targets are presented when implementing the base schedule over the different scenarios. After the pre-stripping years, deviations in the small mill are 18% in average and 22% in the big mill. Regarding the blending element 1 (BEL1) that controls the operation of the small mill,

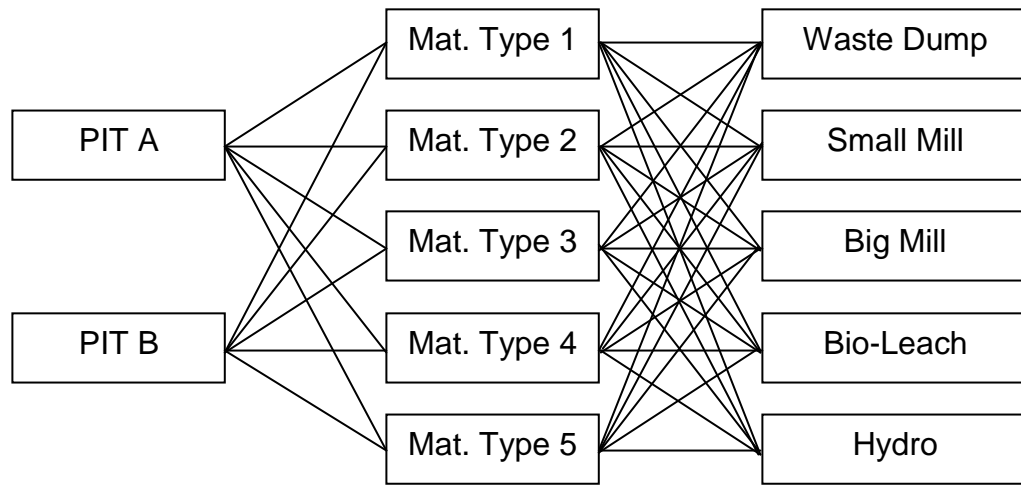


Figure 7: Multipit operation

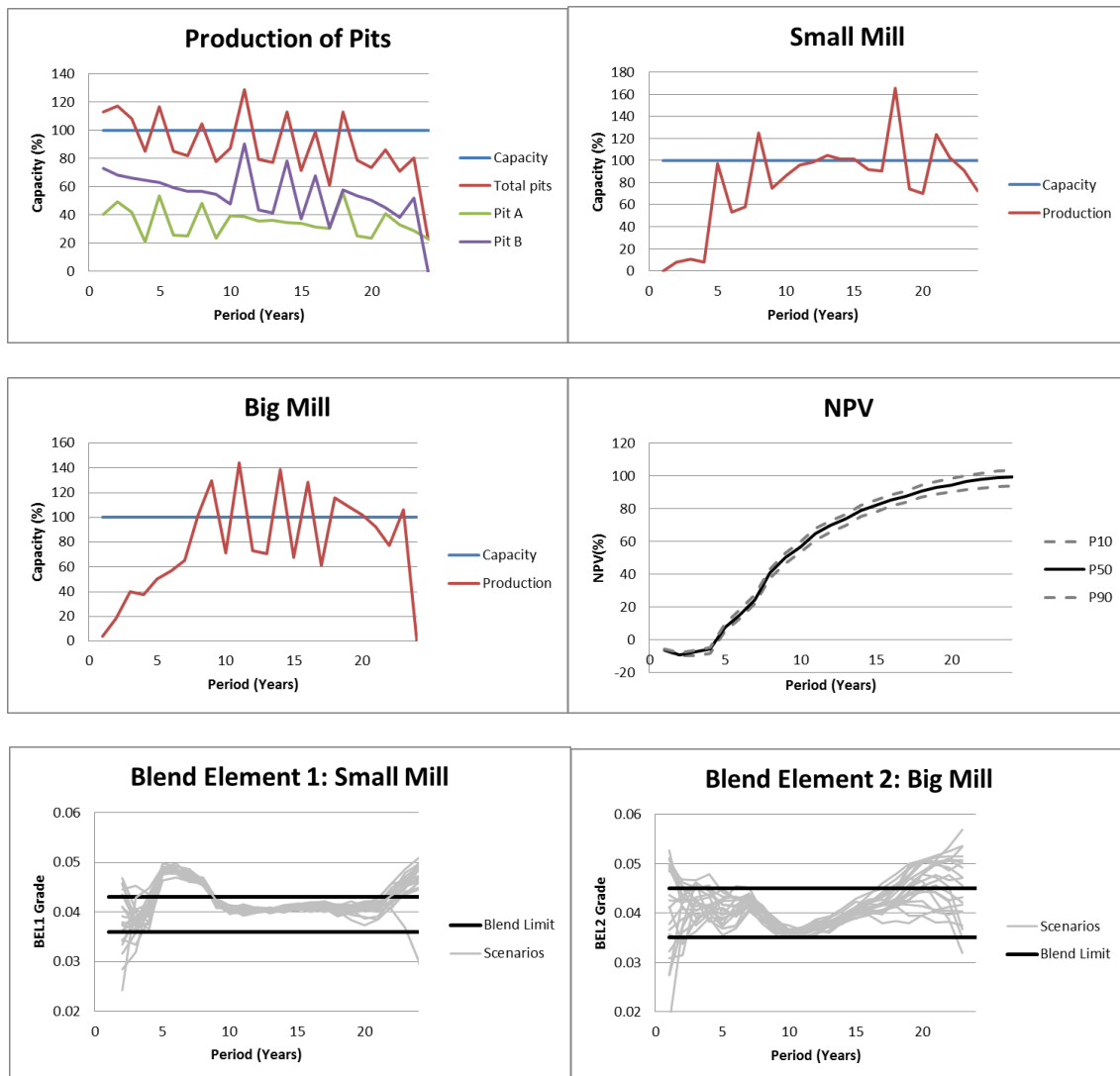


Figure 8: Base case schedule

the deviations in the first 7 years of operation are in average 7%, whereas the blending element 2 (BEL2), that controls the operation of the big mill, deviates in average 1.8% in these periods.

Any conventional scheduler attempts to optimize the sequence of extraction of a given deposit using a single input model. Interpolation methods generate averaged-type models that smooth the grades and do not reproduce the spatial variability of the data. Furthermore, any mining sequence that performs well using an E-type model does not perform well in average with respect to a set of orebody simulations given that the transfer function that relate grades and economic values of blocks is non-linear. These two factors explain the poor performance of deterministic methods when performing risk analysis (Dowd, 1994).

3.3 Optimization parameters

To implement the approach, optimization parameters such as initial temperature, reduction factors, penalties, cycles and number perturbation must be calibrated. The penalties must account for the order of magnitude of the different targets in order to balance the penalization in the objective function. Fig. 9 displays the evolution of the terms of the objective function with the number of perturbations for 5 different temperatures. An initial temperature of 0 means that only perturbations that improve the objective value are accepted (pure iterative improvement) which limits the ability of the methodology of escaping from local optimal solutions. A very large initial temperature implies accepting both, favourable and unfavourable perturbations with high probability, which may not improve the initial solution as the solution will not necessarily converge to a final good solution. It is possible to observe from Fig. 9 that with temperatures between 100.000 and 500.000, the method converges to good solutions in terms of NPV and penalties, whereas with temperatures higher than 1'000.000 the solutions are not improved. It is also observed that an initial temperature of 100.000 provides a better solution in terms of NPV than the pure iterative improvement one given its ability to accept deterioration to explore better the solution domain.

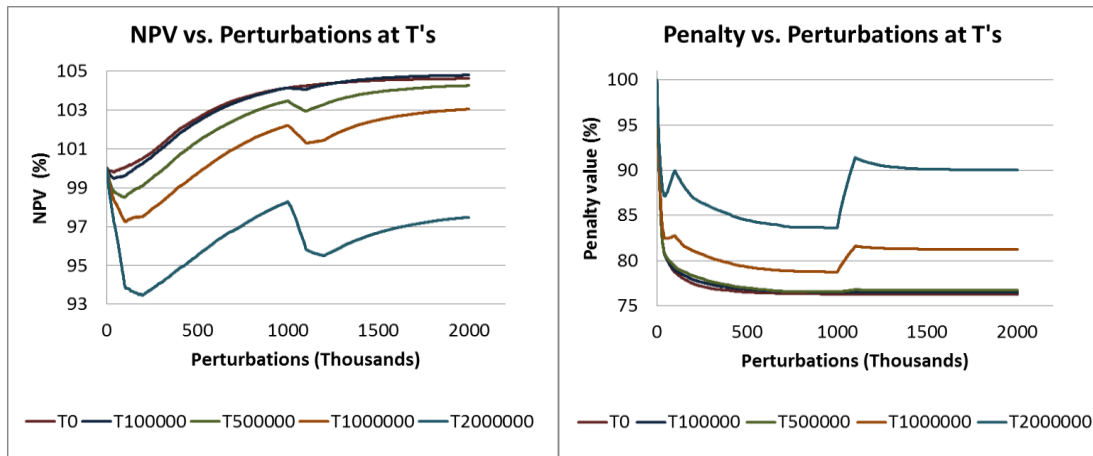


Figure 9: Objective function terms at different temperatures

The same analysis is performed to evaluate the number of cycles (Fig. 10). It can be observed that after two cycles, the improvement in expected NPV is negligible, whereas no significant reduction in penalized deviations is attained after one cycle.

3.4 Case 1: Multipit multiprocessing

The proposed approach is implemented considering the economic and technical parameters used in the base case. The results obtained are displayed in Fig. 11.

Low deviations from capacities and blending targets are expected. After the pre-stripping years, deviations from the capacity of both the small and big mills are 1% on average. The probability of deviating from the

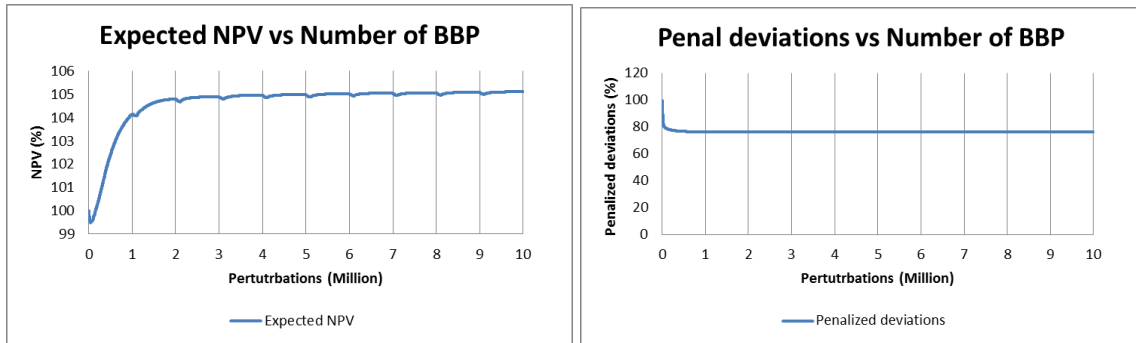


Figure 10: Objective function terms vs. number of cycles

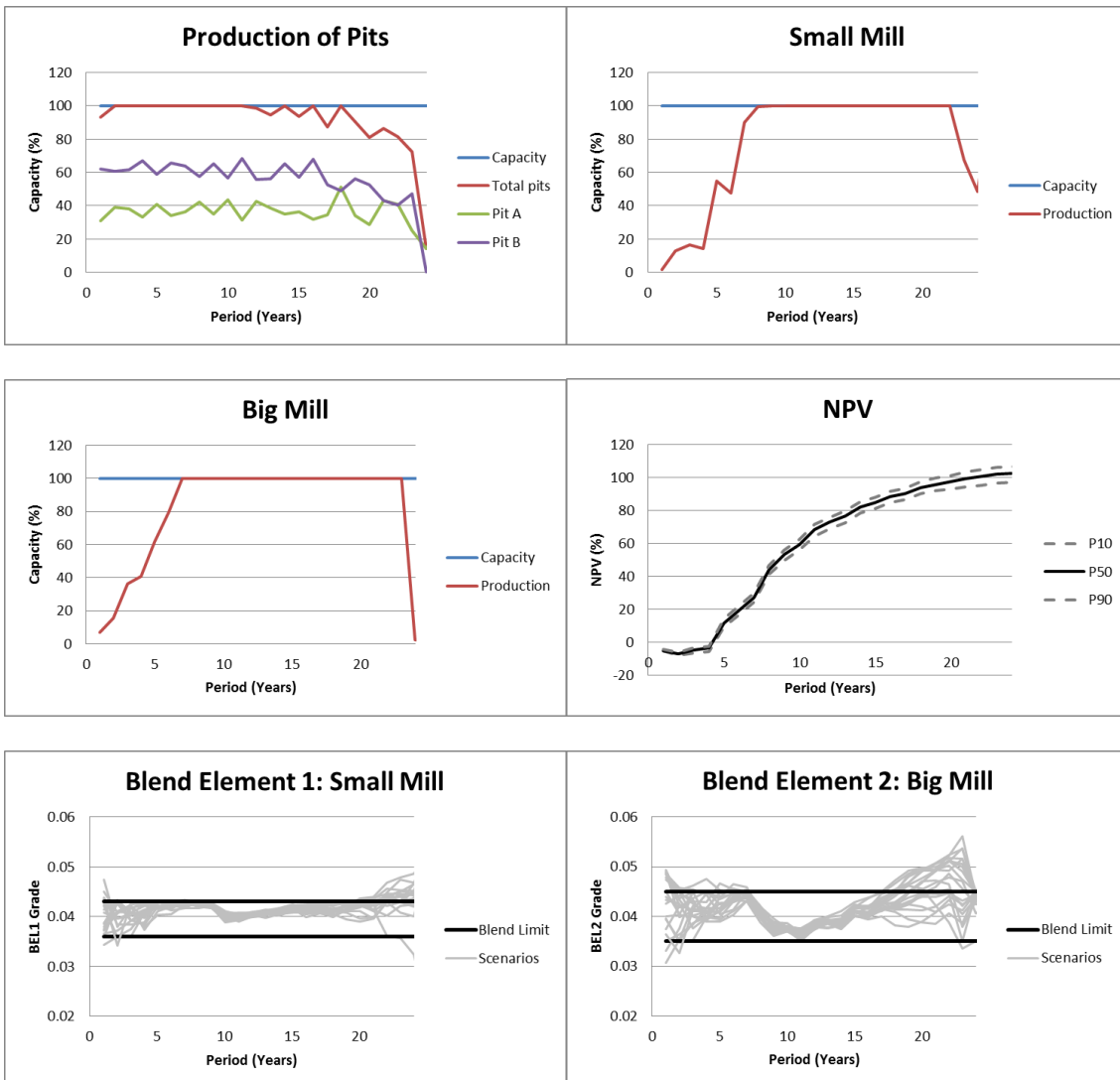


Figure 11: Case 1: Multipit multiprocess

operational ranges of BEL1 are largely reduced, obtaining an average expected deviation of 0.4%. Larger probabilities of deviating are presented at the end, originated from the geological risk discounting applied to the penalties that allow deferring risk to later periods when more information becomes available. For BEL2, there are expected deviations of 1.3%. The expected NPV is 3% higher when compared to the base case; however, given the large and impractical deviation from targets in the base case, its NPV forecast is not reliable.

3.5 Case 2: Multipit multiprocess with operating alternatives at the mills

The method is implemented considering the case where multiple operating alternatives are available in both mills. In case 1, fine grinding option is selected by default. The method is now able to choose which option to implement at each mill along the different periods. For both mills, when operating using a coarse grinding option, the capacities increase by 11.6% and the metallurgical recoveries decrease by 2%. The operational ranges for BEL1 and BEL2 also change with the two different operating alternatives. Given the flexibility in the operation of the mills, the method is able to perform second level perturbations (OAP). Fig. 12 display the results obtained when implementing the method.

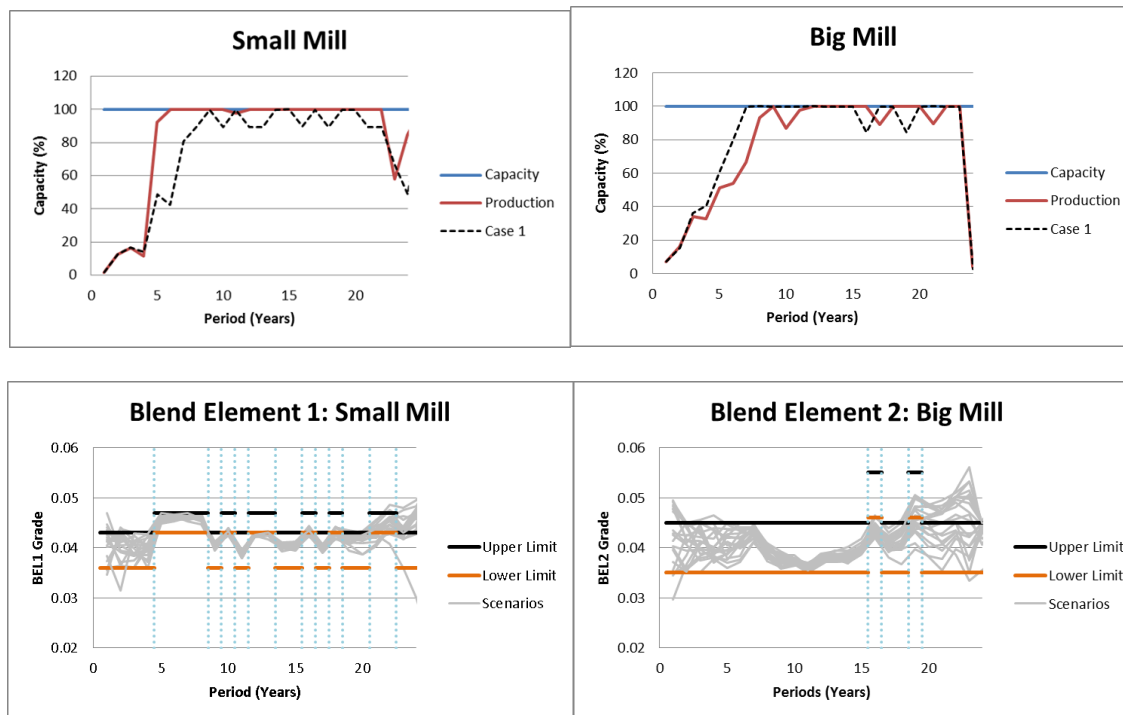


Figure 12: Case 2: Multipit multiprocess with OAs at the mills

The coarse grinding option is selected in years 5–8, 10, 12, 13, 16, 18, 21 and 22 in the small mill, and in years 16, 19 in the big mill. Although capacities of the mill change when swapping from one alternative to another, the algorithm pushes material in a way that deviation from capacities of both mills are well controlled (in average 1% in small mill and 3% in the big mill). The same behaviour is observed with respect to the blend element targets; BEL1 jumps in periods when the small mill operates at coarse grinding to meet the new blending requirements, whereas BEL2 jumps in periods when the big mill swaps to coarse grinding. In average, BEL1 and BEL2 deviate 0.7 and 1.2% respectively.

The risk analysis of the NPV expected by implementing the solution generated in the case 2 is displayed in Fig. 13. This solution generates an expected NPV 5% higher than the base case. As was previously mentioned, the NPV forecasts of the base case solution are not reliable given the large deviations from capacities and

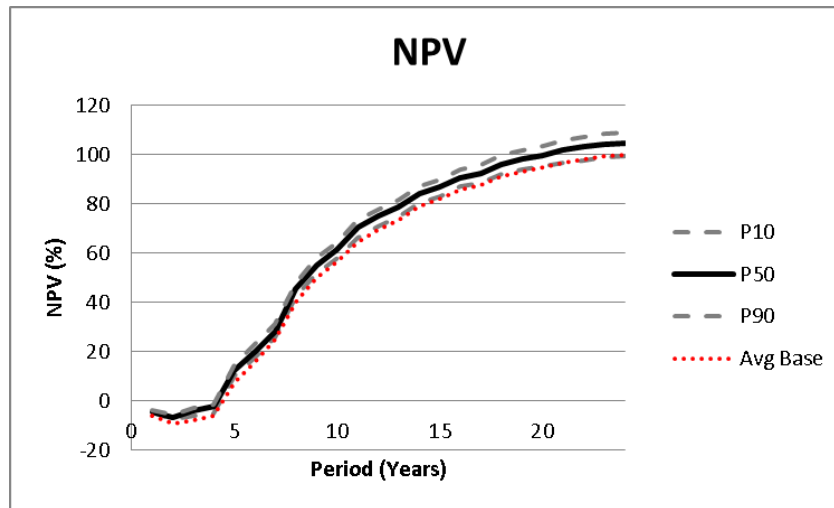


Figure 13: NPV of the case 2 solution

blending targets. The base case solution is improved by means of the two levels of perturbation implemented (BBP and OBP).

4 Conclusions

This paper proposes a method to generate solutions that outperform solutions obtained using conventional deterministic approaches in mining complexes with multiple pits, blending requirements, processing paths, operating alternatives and transportation systems. The solutions generated define the sequence of extraction of the mining blocks in the different pits, the operating alternative implemented at each processing path, and the transportation systems used to carry the processed material to the final stocks.

The implementation of the method in a multipit copper operation allows reducing the average deviations from capacities and blending targets considering an initial solution generated using a conventional optimizer over a single estimated model: from 18 to 1% regarding small mill capacities, from 22 to 3% regarding big mill capacities, from 7 to 0.3% regarding BEL1 in the first 7 periods, and from 1.8 to 0.6% regarding BEL2 in the first 7 periods.

Although NPV forecasts for the base case are not reliable given its large deviations from capacities and blending targets, the solution generated by implementing the proposed method generates an expected NPV 5% higher than the base case, which highlights the ability of the method to generate a higher NPV with less risk.

Future work will seek to find methods that improve the solution's robustness based on the number of scenarios.

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